The Collocation Solution of BVP for a System of ODEs in Photosynthetic Carbon Metabolism Ultimately for Parameter Estimation

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# WHY

# PHOTOSYNTHETIC CARBON METABOLISM?

- 1. THE MOST IMPORTANT BIOLOGICAL PROCESS ON EARTH
  - SURVIVE! Food, hospitable environment & Energy
    - Generate Carbohydrate and oxygen.
      - Photosynthesis Output of Carbohydrate: 160 billion metric tons yearly. = 353200000000 pounds.
- 2. Photorespiration: Not understood completely[26]
- 3. Extended photosynthetic carbon metabolism[20]
  - No current dynamic model of photosynthetic carbon metabolism includes all the reactions in the following.
    - 1. Calvin cycle
    - 2. Photorespiratory metabolism
    - 3. Starch synthesis
    - 4. Suc synthesis





# WHAT PARAMETERS?

- Enzymes for improved crop yield Or increased photosynthetic rate [de Sturler, Zhu, Long]
  - 1. Biotechnology can engineer each enzyme to alter resource allocation between the enzymes
  - 2. 38 enzymes involved in extended photosynthetic carbon metabolism
  - 3. Given a fixed resource of total protein-nitrogen, **10**<sup>9</sup> testing choices for optimal distribution of protein nitrogen into different enzymes.
    - ► WHICH ENZYMES? ► NEED TO IDENTIFY
- The Maximum Rate of some reactions or of all Enzymes in the Photosynthetic Carbon Metabolism
- 7 Proteins that are not necessary for photosynthesis but are required for photorespiration
- Initial Conditions
- Kinetic Constants Used in Rate Equations of each Metabolite[21]

# **PHOTOSYNTHESIS AND ENERGY**

## **2010 The State of the Union**

- "<u>...Continued investment in advanced biofuel..."</u>
- Increase Crop Yield  $\rightarrow$  More Biofuel
- Ethanol Fuel: Fermented sugars from sugar cane, wheat, corn (C4 plants) etc.
- E10: Mandatory in 10 States.

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E85: is used in Sweden. 7 stations in VA (2 open to public), normally 30% cost less than gasoline.
 E100 is widely used in Brazil.

## A SYSTEM OF ODES.

 $\frac{\mathrm{d[RuBP]}}{\mathrm{dt}} = \mathrm{v}_{13} - \mathrm{v}_1 - \mathrm{v}_{111};$  $\frac{d[PGA]}{dt} = 2v_1 - v_2 - v_{32} + v_{111} + v_{113};$  $\frac{d[DPGA]}{dt} = v_2 - v_3;$  $\frac{d[T3P]}{dt} = v_3 - 2v_5 - v_7 - v_8 - v_{10} - v_{31} - v_{33};$  $\frac{\mathrm{d}[\mathrm{FBP}]}{\mathrm{dt}} = \mathrm{v}_5 - \mathrm{v}_6;$  $\frac{d[E4P]}{dt} = v_7 - v_8;$  $\frac{\mathrm{d}[\mathrm{S7P}]}{\mathrm{dt}} = \mathrm{v}_9 - \mathrm{v}_{10};$  $\frac{d[SBP]}{dt} = v_8 - v_9;$  $\frac{d[ATP]}{dt} = v_{16} - v_2 - v_{23} - v_{13} - v_{113};$  $\frac{\mathrm{d}[\mathrm{HexP}]}{\mathrm{dt}} = \mathrm{v}_6 - \mathrm{v}_7 - \mathrm{v}_{23};$  $\frac{d[\text{PenP}]}{dt} = v_7 + 2v_{10} - v_{13};$ 

 $\underline{d[GOAc]} = V_{121} - V_{122} - V_{124}$ đt  $\frac{d[SERc]}{dt} = v_{131} v_{122}$  $\frac{d[GLXe]}{dt} = v_{122} + v_{124} - 2v_{131}$  $\frac{d[HPRc]}{dt} = v_{122} \quad v_{123}$  $\frac{d[GCEAc]}{dt} = v_{123} \cdot v_{1in} + v_{1out}$  $\frac{d[GCEA]}{dt} = v_{1in} - v_{113} - v_{1out}$  $\frac{d[GCA]}{dt} = v_{112} - v_{2out} + v_{2in}$  $\frac{d[PGCA]}{dt} = v_{111} - v_{112}$  $\frac{d[GCAc]}{dt} = v_{2out} - v_{121} - v_{2in}$ 

Where  

$$v_{13} = \frac{V_{13}(ATP \times Ru5P)}{\left(ATP\left(1 + \frac{ADP}{K_{1134}}\right) + K_{M132}\left(1 + \frac{ADP}{K_{1132}}\right)\right) \times \left(Ru5P + K_{M131}\left(1 + \frac{GAP}{K_{1131}} + \frac{RuBP}{K_{1132}} + \frac{Pi}{K_{1133}}\right)\right)$$

$$\vdots$$

$$v_{1} = \frac{RuBP \times W_{c} \times \min\left(1, \frac{RuBP}{E_{r}}\right)}{\left(RuBP + K_{r}\left(1 + \frac{PGA}{K_{111}} + \frac{FBP}{K_{112}} + \frac{SBP}{K_{113}} + \frac{Pi}{K_{114}} + \frac{NADPH}{K_{115}}\right)\right)}; \quad W_{c} = \frac{V_{cmax} \times CO_{2}}{CO_{2} + K_{M11}\left(1 + \frac{O_{2}}{K_{M12}}\right)}$$

$$v_{111} = \frac{RuBP \times W_{o} \times \min\left(1, \frac{RuBP}{E_{r}}\right)}{\left(RuBP + K_{r}\left(1 + \frac{PGA}{K_{111}} + \frac{FBP}{K_{112}} + \frac{SBP}{K_{113}} + \frac{PI}{K_{114}} + \frac{NADPH}{K_{115}}\right)\right)}; \quad W_{o} = \frac{V_{111} \times O_{2}}{O_{2} + K_{o}\left(1 + \frac{CO_{2}}{K_{c}}\right)}$$

# **Stiffness of ODEs**

- Large negative real part of eigenvalues along with others normal magnitude.
- Local Jacobian ,  $\frac{\partial f}{\partial y}$  , has large eigenvalues.
- Need A-Stability Solver or extremely small time steps.
  - IRK\_s (Better Stability with the higher order) = Collocation Method
     × Simple One-Step scheme
- Note that ODE stiff is not related stiffness in parameters as in "Stiff" parameter & "Sloppy" parameter in Gutenkunst[7] and Ashyraliyev[3]

# Implicit S-Stage Runge-Kutta (IRK)

$$y_{i+1} = y_i + h_i \sum_{s=1}^{S} \beta_s f_{is}; \quad 1 \le i \le K.$$
  

$$f_{is} = f\left(t_{is}, y_i + h_i \sum_{l=1}^{S} \alpha_{sl} f_{il}\right) \cdot 1 \le s \le S$$
  

$$t_{is} = t_i + h_i \rho_s; \quad 1 \le s \le S, \quad 1 \le i \le K$$
  

$$f_{is} = f\left(t_{is}, y_{is}\right); \quad y_{is} \coloneqq y_i + h_i \sum_{l=1}^{S} \alpha_{sl} f_{il} = \text{appr of } y(t_{is})$$

with  $0 \le \rho_1 < \rho_2 < \dots < \rho_s \le 1$ . The points  $\rho_s$  are distinct. IRK\_s := This special case of IRK

[1,10

# <sup>12</sup> Construction of Weight For IRK\_s

where aggregate 
$$\alpha$$
 and  $\beta$  are  

$$\sum_{l=1}^{S} \alpha_{sl} = \rho_s. \text{And} \sum_{l=1}^{S} \beta_l = 1. \quad 1 \le s \le S$$
The Butcher Diagram.



# **Collocation Method : ODE Solver**

#### 1. Discretization

- Time domain  $t_0 < t_1 < ... < t_k < ... < t_N$ ,  $I_k = [t_{k-1}, t_k]$ .
- 2. Choose Basis Function:
  - Lagrange Polynomial (for each metabolite and each interval)

$$\begin{split} \tilde{y}_{k,j}(t) &= f\left(l_{k}\right) \frac{\left(t-m_{k}\right)\left(t-r_{k}\right)}{\left(l_{k}-m_{k}\right)\left(l_{k}-r_{k}\right)} + f\left(m_{k}\right) \frac{\left(t-l_{k}\right)\left(t-r_{k}\right)}{\left(m_{k}-l_{k}\right)\left(m_{k}-r_{k}\right)} \\ &+ f\left(r_{k}\right) \frac{\left(t-l_{k}\right)\left(t-m_{k}\right)}{\left(r_{k}-l_{k}\right)\left(r_{k}-m_{k}\right)} \\ &\coloneqq A_{k,j} \frac{\left(t-m_{k}\right)\left(t-r_{k}\right)}{\left(l_{k}-m_{k}\right)\left(l_{k}-r_{k}\right)} + B_{k,j} \frac{\left(t-l_{k}\right)\left(t-r_{k}\right)}{\left(m_{k}-l_{k}\right)\left(m_{k}-r_{k}\right)} + C_{k,j} \frac{\left(t-l_{k}\right)\left(t-m_{k}\right)}{\left(r_{k}-l_{k}\right)\left(r_{k}-m_{k}\right)} \\ &\text{Where } A_{k,j} = f\left(l_{k}\right), B_{k,j} = f\left(m_{k}\right) \& C_{k,j} = f\left(r_{k}\right), \ l,m,r \text{ are timesteps, and } f\left(\cdot\right) \end{split}$$

is a function value at the time.

 $A_{k,j}, B_{k,j}, C_{k,j}$  are unknowns  $\rightarrow 3 \cdot K \cdot J$  unknowns

# Need $3 \cdot K \cdot J$ Equations

- **1.** Left Continuity Condition:  $K \cdot J$
- 2. Right Differentiability Condition: *K* · *J*
- **3.** Collocation Condition: *K* · *J* 
  - Satisfy the given model
    - Highly Nonlinear Equations
    - Need Jacobian

→ 3 · K · J algebraic equations

$$\begin{array}{l} \textbf{Right Differentiability Condition} \\ \Rightarrow (K-1) J \text{ equations} \\ \hline y'_{k,j}(r_k) - \ddot{y}'_{k+1,j}(r_k) = A_{k,j} \frac{(r_k - m_k) + (r_k - r_k)}{(l_k - m_k)(l_k - r_k)} + B_{k,j} \frac{(r_k - l_k) + (r_k - r_k)}{(m_k - l_k)(m_k - r_k)} \\ + C_{k,j} \frac{(r_k - l_k) + (r_k - m_k)}{(r_k - l_k)(r_k - m_k)} - A_{k+1,j} \frac{(r_k - m_{k+1}) + (r_k - r_{k+1})}{(l_{k+1} - m_{k+1})(l_{k+1} - r_{k+1})} \\ - B_{k+1,j} \frac{(r_k - l_{k+1}) + (r_k - r_{k+1})}{(m_{k+1} - l_{k+1})(m_{k+1} - r_{k+1})} - C_{k+1,j} \frac{(r_k - l_{k+1}) + (r_k - m_{k+1})}{(r_{k+1} - l_{k+1})(r_{k+1} - m_{k+1})} = 0. \\ \text{Since } r_k = l_{k+1} \text{ and let } h_k = r_k - l_k \\ \Rightarrow \tilde{y}'_{k,j}(r_k) - \tilde{y}'_{k+1,j}(r_k) = \frac{A_{k,j} - 4B_{k,j} + 3C_{k,j}}{h_k} + \frac{3A_{k+1,j} - 4B_{k+1,j} + C_{k,j}}{h_{k+1}} \end{array}$$

## **Boundary Conditions**

 $\Rightarrow 2J$  equations

• **LBC**  

$$\tilde{y}_{1,j}(l_1) - IC = A_{1,j} \frac{(l_1 - m_1)(l_1 - r_1)}{(l_1 - m_1)(l_1 - r_1)} + B_{1,j} \frac{(l_1 - l_1)(l_1 - r_1)}{(m_1 - l_1)(m_1 - r_1)}$$

$$+ C_{1,j} \frac{(l_1 - l_1)(l_1 - m_1)}{(r_1 - l_1)(r_1 - m_1)} - IC_j$$

$$= A_{-j} - IC_{-j} - 0 \text{ where } IC \text{ represents initial } C$$

 $= A_{1,j} - IC_j = 0$  where *IC* represents initial conditions.

• **RBC** 

$$\begin{split} \tilde{\psi}_{k,j}(r_k) - EC_j &= A_{k,j} \frac{(r_k - m_k)(r_k - r_k)}{(l_k - m_k)(l_k - r_k)} + B_{k,j} \frac{(r_k - l_k)(r_k - r_k)}{(m_k - l_k)(m_k - r_k)} \\ &+ C_{k,j} \frac{(r_k - l_k)(r_k - m_k)}{(r_k - l_k)(r_k - m_k)} - EC_j \end{split}$$

 $= C_{k,j} - EC_j = 0$  where EC represents end conditions.

# **Collocation Condition**

# $\vec{y}_{k,j}'(m_k) = A_{k,j} \frac{(m_k - m_k) + (m_k - r_k)}{(l_k - m_k)(l_k - r_k)} + B_{k,j} \frac{(m_k - l_k) + (m_k - r_k)}{(m_k - l_k)(m_k - r_k)}$ $+ C_{k,j} \frac{(m_k - l_k) + (m_k - m_k)}{(r_k - l_k)(r_k - m_k)} = f(m_k, \tilde{y}(m_k))$ $\Rightarrow \dot{\tilde{y}}_{k,j}(m_k) - f(m_k, \tilde{y}(m_k)) = 0$

For example: (Equidistance Case)

$$\tilde{y}_{k,j}'(m_k) = A_{k,j} \frac{\left(-\frac{h_k}{2}\right)}{\left(-\frac{h_k}{2}\right) \cdot \left(-h_k\right)} + B_{k,j} \frac{\left(\frac{h_k}{2}\right) + \left(-\frac{h_k}{2}\right)}{\left(\frac{h_k}{2}\right) \cdot \left(-\frac{h_k}{2}\right)} + C_{k,j} \frac{\left(\frac{h_k}{2}\right)}{\left(h_k\right) \cdot \left(\frac{h_k}{2}\right)}$$

$$\tilde{y}_{k,j}'(m_k) = A_{k,j} \frac{1}{\left(-\frac{h_k}{2}\right) \cdot \left(-h_k\right)} + B_{k,j} \frac{\left(\frac{h_k}{2}\right) \cdot \left(-\frac{h_k}{2}\right)}{\left(\frac{h_k}{2}\right) \cdot \left(-\frac{h_k}{2}\right)} + C_{k,j} \frac{\left(\frac{h_k}{2}\right)}{\left(h_k\right) \cdot \left(\frac{h_k}{2}\right)}$$

$$\tilde{y}_{k,j}'(m_k) = A_{k,j} \frac{1}{(-h_k)} + C_{k,j} \frac{1}{(h_k)} = \frac{k,j}{h_k} = f(m_k, y(m_k))$$

# **Automatic Differentiation (AD)**

- Systematic application of the chain rule.
- "NUMERICALLY EXACT evaluation of derivatives" Shampine, Kierzenka, Forth (2005)
- Accurate to within roundoff.
- No Discretization or Cancellation errors Unlike FD
   ADMAT/ADMIT: Verma, Coleman
  - MAD AD: Forward Mode AD [Forth, 2006].
    - × Quicker w/AD than w/o AD for vectorized cases\*.
  - ADIMAT: Vehreschild [18]
    - **×** Forward AD: Directional derivatives and its Value calculated
    - × More efficient than other AD [Forth, 2006]

# Jacobian Structure Comparison for Solving Nonlinear equations. FD vs. AD





# **Data VS Collocation Solutions (K=3)**



**CM8** 

# **Data VS Collocation Solutions I (K=20)**



#### CM9

# Solving Non-Linear K=3000



# **Error Control and Adaptive Refinement**

- 1.Order *p* : Truncation error  $\tau_{i+1}(h)$
- 2.Order p + 1: Truncation error  $\hat{\tau}_{i+1}(h) = O(h^{p+1})$
- Assume  $\tilde{y}_i \approx y(t_i) \approx \hat{y}_i$ .  $\tau_{i+1}(h_i) = \frac{y(t_{i+1}) - y(t_i)}{h_i} - \phi(t_i, y(t_i), h) = \frac{y(t_{i+1}) - \tilde{y}_i}{h_i} - \frac{h_i \phi(t_i, y(t_i), h)}{h_i}$  $=\frac{y(t_{i+1})-\left[\tilde{y}_{i}+h_{i}\phi(t_{i},y(t_{i}),h)\right]}{h}=\frac{y(t_{i+1})-\tilde{y}_{i+1}}{h}$ Similarly,  $\hat{\tau}_{i+1}(h_i) = \frac{y(t_{i+1}) - \hat{y}_{i+1}}{h}$ , but  $\tau_{i+1}(h_i) = \frac{y(t_{i+1}) - \tilde{y}_{i+1}}{h} = \frac{y(t_{i+1}) - \hat{y}_{i+1}}{h}$  $=\frac{y(t_{i+1})-\hat{y}_{i+1}+(\hat{y}_{i+1}-\tilde{y}_{i+1})}{h}=\hat{\tau}_{i+1}(h)+\frac{\hat{y}_{i+1}-\tilde{y}_{i+1}}{h}\approx\frac{\left[\hat{y}_{i+1}-\tilde{y}_{i+1}\right]}{h}=h_i^{-1}\left[\hat{y}_{i+1}-\tilde{y}_{i+1}\right]$

3. Given Step Size  $h_i$ , accept the step if  $|\hat{y}_{i+1} - \tilde{y}_{i+1}| \le h_i Tol$ 

# **Nonlinear Least-Squares Problem**

- 1. Collocation Approximation Solution.
- 2. Data

3. Minimize the Residual (Discrepancy btn 1 & 2).

The Gauss-Newton Method.

The Levenberg-Marquardt Method

Optimized Parameters.

# Why Difficult? Issues?

Jacobians : Solving nonlinear equation & optimization.

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• Exploit Structures of Jacobians:

- **×** Banded FD, Block FD.
- **×** Coll Cond : ADiMat.
- Vectorization is used for Jacobian build for speed.
- Ill-Conditioned Jacobian.
  - Used different basis functions
- Stiffness of ODE:
- Sloppiness of Parameters.
- A Few Unstable Metabolites  $\rightarrow$  Error  $\uparrow$

• Adaptive Step Size Refinement.

# What To Do



- More efficient & robust algorithm
  - as a method of parameter estimation for broader practical applications.
  - Acceleration techniques to improve the accuracy:
- Parameter Correlation
  - Assumed zero parameter correlation now
- Combining deterministic and stochastic parameter estimation for the same model

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