On the accuracy of the rotation form in simulations of the Navier-Stokes equations

Leo Rebholz

rebholz@clemson.edu

Department of Mathematical Sciences Clemson University Clemson, SC 29634



Leo Rebholz, Clemson University – p. 1/?

Outline

- Joint work with W. Layton, C. Manica, M. Neda and M. Olshanskii
- NSE and its nonlinearity
- Discrete nonlinearity forms: convective, skew-symmetric, rotational
- Examples that show drastic differences; rotational form bad!
- Discussion of possible cause
- **Fix** proposed: Grad-div stabilization
- **Examples that show fix works**



Navier-Stokes equations

NSE in convective form

$$u_t + u \cdot \nabla u + \nabla p - Re^{-1}\Delta u = f, \ \nabla \cdot u = 0$$

Vector identity:

<u>ll+</u>

$$u \cdot \nabla u = -u \times (\nabla \times u) + \frac{1}{2} \nabla |u|^2$$

Using Bernoulli pressure $\tilde{p} = p + \frac{1}{2} |u|^2$, NSE in rotational form given by

$$u \times (\nabla \times u) + \nabla \tilde{p} - Re^{-1}\Delta u = f, \ \nabla \cdot u = 0$$

FEM scheme for NSE

■ Naive Crank-Nicolson FEM scheme for NSE w/ convective form of NSE: $\forall (v_h, q_h) \in (X_h, Q_h)$

$$\frac{1}{\Delta t}(u_{h}^{n+1} - u_{h}^{n}, v_{h}) + (u_{h}^{n+1/2} \cdot \nabla u_{h}^{n+1/2}, v_{h}) \\ -(p_{h}^{n+1/2}, \nabla \cdot v_{h}) + Re^{-1}(\nabla u_{h}^{n+1/2}, \nabla v_{h}) = (f(t^{n+1/2}), v_{h}) \\ (\nabla \cdot u_{h}^{n+1}, q_{h}) = 0$$

• This scheme known to be unstable



Variations of NSE scheme

For stability, scheme often altered
Skew symmetric form:

$$(u_h \cdot \nabla u_h, v_h) \rightarrow \frac{1}{2}(u_h \cdot \nabla u_h, v_h) - \frac{1}{2}(u_h \cdot \nabla v_h, u_h)$$

Rotational form:

$$(u_h \cdot \nabla u_h, v_h) - (p_h, \nabla \cdot v_h) \rightarrow - (u_h \times (\nabla \times u_h), v_h) - (\tilde{p}_h, \nabla \cdot v_h)$$

In continuous case all 3 forms are equivalent



Variations of NSE scheme

For both skew symmetric and rotational form schemes, we can prove

$$\|u_h^M\|^2 + \nu \Delta t \sum_{n=0}^{M-1} \|\nabla u_h^{n+1/2}\|^2 \le C(Re, f, T, u_0)$$

- **So** both schemes are stable and conserve energy
- There are situations where one may want to use the rotational form scheme instead of convective form
 - Conservation of helicity
 - More robust preconditioners for large Reynolds numbers available





Channel Flow around a cylinder benchmark problem Domain:



The time dependent inflow and outflow profile are

$$u_1(0, y, t) = u_1(2.2, y, t) = \frac{6}{0.41^2} \sin(\pi t/8) y(0.41 - y)$$
$$u_2(0, y, t) = u_2(2.2, y, t) = 0.$$

No slip boundaries, 0 initial condition, $0 \le Re(t) \le 100$.

From (P_2, P_1) skew-symm scheme at t=4,5,6,7 (Good!)





(P_2, P_1) rotational form, same mesh, t=4,5,6,7 (Bad!)





- **How can we get such different answers**? Increased pressure error for rotational form $\tilde{p} = p + \frac{1}{2} |u|^2$ more complex than p Boundary layers in Bernoulli pressure **On meshes where** p_h is resolved, \tilde{p}_h may not be For (P_k, P_{k-1}) elements, "some of u" gets approximated with P_{k-1} for Bernoulli pressure **Roughly speaking, if this pressure term is dominant,** velocity error scales with Re * pressure error
 - Similar problem in Stokes equations can be fixed with grad-div stabilization (Olshanskii/Reusken)
 Analysis of pressure term same in Stokes and NSE...

Consider Stokes problem, where there is same pressure term on RHS of velocity error equation

$$-Re^{-1}\Delta u + \nabla p = f, \ \nabla \cdot u = 0 \text{ in } \Omega$$
$$u = 0 \text{ on } \partial \Omega$$

FEM scheme: $\forall v_h \in X_h, q_h \in Q_h$, solve

$$Re^{-1}(\nabla u_h, \nabla v_h) - (p_h, \nabla \cdot v_h) + (q_h, \nabla \cdot u_h) = (f, v_h)$$
$$(\nabla \cdot u_h, q_h) = 0$$



Typical velocity error bound for scheme:

$$\begin{aligned} \|\nabla(u-u_h)\| &\leq C(\inf_{v\in X_h} \|\nabla(u-v_h)\| + Re\inf_{q_h\in Q_h} \|p_h-p\|) \\ &\leq Ch^2(\|\nabla\nabla u\| + Re*\|\nabla p\|) \end{aligned}$$

 Olshanskii / Reusken: Add grad-div stabilization, γ(∇ · u_h, ∇ · v_h) to LHS of FEM scheme for Stokes equations, with γ = O(1).
 New error equation:



$$(u - u_h) \| \le Ch^2 \sqrt{Re} (\|\nabla \nabla u\| + \|\nabla p\|)$$

In short, the grad div term lets you handle $\inf_{q_h \in Q_h} \|p - q_h\| \|\nabla \cdot (u_h - U)\| \text{ in a different way}$

Without stabilization, you have to "hide" the $\|\nabla \cdot (u_h - U)\|$ part on the left hand side in the $Re^{-1}\|\nabla (u_h - U)\|^2$ term

Creates a $Re * \inf_{q_h \in Q_h} ||p - q_h||^2$ on the RHS

With stabilization, will have a $\|\nabla \cdot (u_h - U)\|^2$ on the LHS, and so only a $\inf_{q_h \in Q_h} \|p - q_h\|^2$ will be left on the RHS

Dependence of velocity error on pressure error is greatly reduced.



From (P_2, P_1) grad-div stabilized rotational form at t=4,5,6,7 (Good!)





- Second test problem: Benchmark channel flow over a step
- **FreeFem**, (P_2, P_1) elements
- **Re**=600
- Dirichlet parabolic inflow, do-nothing outflow
- No slip sides
- Eddies should form behind step, detach, and new ones should form



NSE with skew-symmetric form of nonlinearity





Leo Rebholz, Clemson University – p. 16/?

NSE w/ rotational form of nonlinearity





Leo Rebholz, Clemson University – p. 17/2

NSE w/ rotational form and grad-div stabilization; unresolved issue w/ what is correct outflow bdry condition











Conclusions

- There are cases where skew-symmetric FEM scheme tends to be much more accurate than rotational form scheme
- Difference is due to increased error in Bernoulli pressure, which in turn increases velocity error
- Adding grad-div stabilization can lessen the effect, especially for higher Re, thus reducing error in velocity field
- We are NOT claiming rotation + grad-div is best, but if you want to use rotational form, adding grad-div can greatly improve accuracy.

